

ENGLISH TRANSLATION OF  
INTERNATIONAL APPLICATION  
AS ORIGINALLY FILED

## DESCRIPTION

ELECTRICAL CONTACT COMPONENT, COAXIAL CONNECTOR, AND  
ELECTRICAL CIRCUIT DEVICE INCLUDING THOSE COMPONENTS

### Technical Field

The present invention relates to a surface-mount electrical contact component, such as a coaxial connector, and an electrical circuit device including the same.

### Background Art

Some of the electrical circuit devices, such as communication devices of cellular phones, conventionally include a signal-switchable surface-mount coaxial connector having a switch. For example, Patent Document 1 has disclosed one of such coaxial connectors.

Fig. 4 shows the general appearance of the surface-mount coaxial connectors, and Fig. 5 shows its cross section. The coaxial connector 10 includes an external terminal 2, an input terminal 3, and a fitting portion 4. The external terminal 2 has a first principal surface 11 opposing a wiring board 31, a second principal surface 12 substantially parallel to the first principal surface 11, and a pair of sides 13. The boundary between the second principal surface 12 and the sides 13 is defined by an edge line 14. The external terminal 2 has a base form. The fitting portion 4

is provided in a cylindrical form on the second principal surface 12 of the external terminal 2 and integrated with the external terminal 2.

The surfaces of the external terminal 2, input terminal 3 and fitting portion 4 are covered with metal films by, for example, plating, and the external terminal 2 and the fitting portion 4 are electrically connected to each other. The metal films each include an underlayer made of a Ni metal film 42 and a surface layer made of a Au metal film 43.

The coaxial connector 10 will be surface-mounted on the wiring board 31 with solder. More specifically, the external terminal 2 and the input terminal 3 are electrically connected to predetermined positions of the wiring board 31, thereby achieving the function as the coaxial connector. Fig. 5 is a sectional view of the mounted coaxial connector taken along a plane perpendicular to the sides 13, omitting the internal structure including the input terminal 3.

In use of the coaxial connector 10, unfortunately, the solder 32 applied for surface mounting to connect the external terminal 2 spreads on and rises from the second principal surface 12, and further reaches the fitting portion 4 as shown in Fig. 5. Consequently, fitting failure may occur in the socket of the coaxial cable corresponding to the fitting portion 4. Although it suffices that the

solder 32 reaches the sides 13 of the external terminal 2, the solder 32 that has risen to the second principal surface 12 easily reaches the fitting portion 4.

The surface mounting of the coaxial connector 10 is generally performed by passing it through a reflow furnace, and this is often repeated several times. Consequently, solder deposited at appropriate positions may be remelted by repetition of the passing through the reflow furnace and thus disadvantageously rise and reach the fitting portion 4.

In order to prevent the solder from rising, Patent Document 2 has disclosed a method for forming an oxide coating film over a predetermined region.

In Patent Document 3, for the formation of the Au plating surface layer on the Ni plating underlayer, a region where the Au plating layer is not formed is prepared and the Ni plating layer exposed at this region is oxidized by an alkaline aqueous solution so that the oxidized Ni film prevents the solder from rising.

In Patent Document 4, a metal film having a low solder wettability is formed as the underlayer and another metal film having a high solder wettability is formed as the surface layer over the underlayer. Then, only a specific region of the metal surface layer is removed by etching, so that the exposed metal film having a low solder-wettability prevents the solder from rising.

Unfortunately, the method disclosed in Patent Document 2 requires the additional step of forming the oxide coating film after the steps of forming the metal films. This disadvantageously makes the manufacture process complicated.

In the method disclosed in Patent Document 3, the step of forming a resist layer or a mask layer so as not to form the Au plating film in a specific region is complicated, and besides the step of oxidation treatment with an alkaline treating agent is complicated.

In the method disclosed in Patent Document 4, the step of etching by laser exposure is complicated and is of high cost.

[Patent Document 1] Japanese Unexamined Patent Application Publication No. 2001-176612

[Patent Document 2] Japanese Unexamined Patent Application Publication No. 8-213070

[Patent Document 3] Japanese Unexamined Patent Application Publication No. 10-247535

[Patent Document 4] Japanese Unexamined Patent Application Publication No. 2002-203627

Disclosure of Invention

Problems to be Solved by the Invention

In view of the above-described disadvantages, the object of the present invention is to prevent fitting

failure caused by the rise of solder used for surface mounting of the electrical contact components, such as coaxial connectors, at low cost without complicated steps.

#### Means for Solving the Problems

Accordingly, the present invention provides an electrical contact component including: a base to be mounted on a surface of a mounting board with a solder, the base having a first principal surface opposing the surface of the mounting board, a second principal surface substantially parallel to the first principal surface, and sides substantially perpendicular to the first and second principal surfaces and connecting the first principal surface to the second principal surface; and a fitting portion continuously provided on the second principal surface, the fitting portion having a fitting periphery forming a tubular shape,

wherein the fitting periphery of the fitting portion is electrically connected to the second principal surface and the sides of the base by metal films formed over their respective surfaces, and

wherein the metal films each include a first metal layer containing Ni as a principal constituent and Co, and a second metal layer containing Au as a principal constituent and overlying the first metal layer.

When the electrical contact component according to the present invention is mounted on a board, the constituents (Ni, Co) of the first and the second metal layer diffuse into the solder that has risen along the sides of the base, and chemically react with Sn being the principal constituent of the solder to produce an intermetallic compound. The Co promotes the diffusion of the Ni into the solder. This intermetallic compound prevents the solder from rising to the second principal surface.

Preferably, the base of the electrical contact component serves as an external terminal and is integrated with the fitting portion, and the second principal surface is partitioned from the sides by an edge line.

Preferably, the first and the second metal layer are formed by plating or cladding. The Co content in the first metal layer is preferably in the range of 5 to 80 percent by weight, and more preferably 10 percent by weight or more.

The electrical contact component according to the present invention can be represented by a coaxial connector having a cylindrical fitting portion formed on the second principal surface of the external terminal.

The electrical contact component represented by the coaxial connector and a wiring board on which the base is surface-mounted with a Sn-based solder constitute an electrical circuit device, such as a communication device.

## Advantages

In the electrical contact component of the present invention, the change of the constituent of the metal film serving as the underlayer can prevent the solder from excessively rising and the fitting failure of sockets and other parts. Accordingly, no complicated step is required, and thus the cost can be reduced.

## Brief Description of the Drawings

Fig. 1 is a perspective view of a coaxial connector being an example of the electrical contact component according to the present invention.

Fig. 2 is a sectional view of the coaxial connector mounted on a wiring board.

Fig. 3 is a photograph of a mounted test piece in an example of the present invention, viewed from above.

Fig. 4 is a perspective view of a known coaxial connector.

Fig. 5 is a sectional view of the known coaxial connector mounted on a wiring board.

Fig. 6 is a photograph of a mounted test piece in a comparative example, viewed from above.

## Best Mode for Carrying Out the Invention



An embodiment of the electrical contact component according to the present invention will now be described using a coaxial connector.

Fig. 1 shows the appearance of a coaxial connector 1 being an embodiment of the present invention, and Fig. 2 shows its cross section. The appearance and the basic structure of the coaxial connector 1 are the same as those of the generally known coaxial connector shown in Figs. 4 and 5, but different only in constituent of the first metal layer 22 serving as the underlayer.

Fig. 2 is a sectional view of the coaxial connector 1 surface-mounted on a wiring board 31. The section is taken along a plane perpendicular to the sides 13 of the external terminal 2, and the input terminal 3 and the internal parts of the coaxial connector are not shown.

The coaxial connector 1 includes an external terminal 2, an input terminal 3, and a fitting portion 4. Since the external terminal 2 and the input terminal 3 will be connected to the land of the wiring board 31 with solder 32 for surface mounting on the wiring board 31, they are located in positions that can be brought into contact with the wiring board 31. The external terminal 2 is a base having a first principal surface 11 opposing the wiring board 31, a second principal surface 12 substantially parallel to the first principal surface 11, and a pair of

sides 13. For the proper function as the coaxial connector, the external terminal 2 and the input terminal 3 are electrically isolated from each other, and the external terminal 2 and the fitting portion 4 are electrically connected to each other and hence integrated with each other.

The external terminal 2 is partitioned into the substantially horizontal second principal surface 12 and the sides 13. The words "substantially horizontal" mean that the surface is substantially parallel to the surface of the wiring board 31. This surface is not necessarily precisely parallel, and may slightly tilt as long as the coaxial connector 1 ensures its function. The sides 13 have surfaces to be wetted by the solder used for mounting and are physically connected to the wiring board 31. The sides 13 are defined by two opposing faces of the four faces perpendicular to the substantially horizontal principal surface 12 of the external terminal 2. These two sides 13 may extend to the other two faces. The sides 13 are not necessarily precisely perpendicular to the wiring board 31, and may slightly tilt unless a problem is caused by mounting. The edge line 14 is appropriately chamfered.

The fitting portion 4 of the coaxial connector 1 is typically cylindrical as shown in Fig. 1. The fitting portion 4 is however not necessarily cylindrical as long as it can fit into, for example, a socket. For example, the

fitting portion 4 can be in a prism-like form. The fitting portion 4 shown in Fig. 1 protrudes from the second principal surface 12 and whose periphery fits with, for example, the socket. The fitting portion may extend downward; hence, the second principal surface 12 has a hole for fitting. Also, the fitting portion 4 may be screw-fitted with, for example, the socket.

The surfaces of the external terminal 2, the input terminal 3 and the fitting portion 4 are coated with a metal film. In Fig. 2, first, a first metal layer 22 mainly containing Ni is formed as an underlayer over the base material 21 of these portions. Then, a second metal layer 23 mainly containing Au is formed as a surface layer. The first metal layer 22 and the second metal layer 23 may be separated by another metal layer unless the object of the present invention is hindered. However, the first metal layer 22 and the second metal layer 23 suffice to accomplish the object of the present invention, and an additional layer is not particularly required.

It is important for the surface layer, or the second metal layer 23, to have a high solder wettability, and accordingly the second metal layer mainly contains Au. The Au coating film is not degraded by sulfuration, unlike Ag coating films. A small amount of impurities may be contained as long as sufficient solder wettability is

ensured.

The present invention features a constituent of the first metal layer 22. Specifically, the first metal layer 22 contains Ni as a principal constituent and an appropriate amount of Co. Consequently, the first metal layer can prevent the solder used for mounting from rising to the second principal surface 12 and further reaching the fitting portion 4, effectively in comparison with the known Co-free Ni metal layer, as described below. The first metal layer 22 is required to have a high adhesion to the second metal layer 23. The Co-containing Ni-based metal layer 22 satisfies this requirement. The first metal layer 22 may contain another constituent or impurities unless the object of the present invention is hindered.

As for the Co content in the first metal layer 22, if the passing through the reflow furnace is performed 3 times, a Co content of less than 5 percent by weight undesirably results in an insufficient effect in preventing the solder from rising. Preferably, the Co content is 5 percent by weight or more. A Co content of 10 percent by weight or more is much preferable and produces a satisfactory effect in preventing the solder from rising even if the passing for reflow is performed 5 times. However, if the Co content is more than 80 percent by weight, many voids can be formed in solder fillets to reduce the bonding strength.

The base material 21 of the external terminal 2, the input terminal 3 and the fitting portion 4 can be made of, but not limited to, metal, resin, or ceramic. If the base material 21 is mainly made of Ni containing Co, the base material 21 can produce the same effect as the first metal layer 22.

The process for manufacturing the coaxial connector 1 will now be described. In this section, only the formation of the first metal layer 22 and the second metal layer 23 will be described. The coaxial connector 1 is manufactured in the same process as the known coaxial connector.

One of the techniques for forming the first metal layer 22 and the second metal layer 23 is plating, which is a conventional process. If the base material 21 is made of a metal, electrolytic plating is preferably employed. First, a bare base material 21 and an electrically conductive medium are placed in a plating bath containing Ni and Co ions, and a current is applied to deposit Ni and Co over the surface of the base material 21, with the plating bath stirred. A Ni metal layer containing Co, that is, the first metal layer 22, is thus formed. Then, the resulting base material is placed in a plating bath containing Au ions and a current is applied to form a Au metal layer, that is, the second metal layer 23, over the surface of the first metal layer 22, with the plating bath stirred.

The above-described plating may be performed by electroless plating. For example, a bare base material 21 is placed in a plating bath containing Ni and Co ions. A reducing agent in the plating bath causes a reduction reaction so that Ni and Co are deposited over the surface of the base material 21 to form the first metal layer 22. Then, the resulting base material is placed in a plating bath containing Au ions. The difference between the Ni and Co immersion potential and the Au deposition potential causes a substitution reaction, and consequently forms a Au metal layer, that is, the second metal layer 23, over the surface of the first metal layer 22.

The first metal layer 22 and the second metal layer 23 may be formed by cladding. First, a plate being the base material 21 and a Ni plate containing Co are laid over each other and pressed and rolled to be integrated, thus forming a clad material. The clad material is pressed into the form shown in Fig. 1, in such a manner that the Co-containing Ni layer defines the surface. Thus, the surface of the base material 21 is covered with the first metal layer 22. Subsequently, the Au-based second metal layer 23 is formed by the above-described plating. Thus, a coaxial connector having the same function as that manufactured by the above-described plating can be produced.

The clad material may be composed of three layers

expressed by base material/Co-containing Ni/Au. In this instance, no Au plating step is required. Cladding can more reduce the variation in Co content than plating, and accordingly the variation of solder rising can be reduced. Furthermore, cladding makes the plating step unnecessary or reduced. Thus, negative effects on environment can advantageously be reduced.

If the base material 21 contains the same constituents as the first metal layer 22, the first metal layer 22 does not need to be provided separately by plating or cladding and only the second metal layer 23 may be formed.

The following will describe the phenomenon produced when the coaxial connector 1 is surface-mounted on a wiring board 31, and a mechanism for preventing the solder from rising, with reference to Fig. 2.

When the coaxial connector 1 is surface-mounted on a wiring board 31 with solder 32, a heating step is performed using a reflow furnace or the like. The solder 32 is melted and solidified, so that the coaxial connector 1 is electrically and physically connected to the wiring board 31. How the solder 32 wets the sides 13 of the external terminal 2 will be described here. The solder 32 forms fillets at the sides 13 as shown in Fig. 2 to bond to the wiring board 31. The solder mainly contains Sn.

When the Sn-based solder is heated to melt and wets the

sides 13, the constituents of the first metal layer 22 and second metal layer 23 forming the surface of the sides 13 diffuse into the solder 32. In particular, the constituents of the first metal layer 22, that is, Ni and Co, diffuse into the solder 32 and react with Sn being the principal constituent of the solder 32 to produce an intermetallic compound 33 of Sn/Ni or Sn/Ni/Co. The Co can promote the diffusion of Ni into the solder 32.

The intermetallic compound 33 has a higher melting point than the Sn-based solder 32, and is difficult to remelt even by repeatedly passing through a reflow furnace several times. The intermetallic compound 33 therefore blocks the flow of the solder 32 melted or remelted for mounting in the vicinity of the edge line 14, and thus prevents the solder 32 from rising to the second principal surface 12. Thus the solder 32 does not reach the fitting portion 4.

If a Pb-free Sn-Ag-based solder is used as the solder 32, the temperature of the heating step must be higher because the melting point of the Pb-free Sn-Ag-based solder is at least 40°C higher than that of Sn-Pb-based solder, or generally used eutectic solder. Higher temperature promotes the diffusion of the Ni, and further enhances the effect of Co of promoting the diffusion of the Ni. This multiplier effect prevents the solder from rising more effectively.



The intermetallic compound 33 does not reduce the bonding strength between the coaxial connector 1 and the wiring board 31.

Accordingly, the electrical contact component represented by the coaxial connector 1 can prevent fitting failure resulting from excessive rise of solder at low cost without complicated process steps, by adding Co to the Ni-based first metal layer 22.

The electrical contact component of the present invention surface-mounted on the wiring board is useful for electrical circuit devices, such as communication devices.

#### EXAMPLES

Examples of the electrical contact component of the present invention will now be described, using coaxial connectors having the same structure as in Figs. 1 and 2.

First, a plate mainly made of brass was pressed to form a test piece of the coaxial connector having the external terminal 2, the input terminal 3, and the fitting portion 4. The details for designing and forming the structure shown in Fig. 1, which are the same as in the general method as disclosed in Patent Document 1, are omitted.

The bare pressed base material 21 and an electroconductive medium were placed in a plating bath containing Ni and Co ions, and a current was applied to form

the first metal layer 22 over the surface of the base material 21, with the plating bath stirred. The amounts of Ni and Co ions in the plating bath were controlled so that the Co content x by weight in the first metal layer 22 would be the values shown in Table 1. The thickness was 1.2  $\mu\text{m}$ .

Then, the test piece having the first metal layer 22 was placed in a plating bath containing Au ions, and a Au film serving as the second metal layer 23 was formed over the first metal layer 22 with the plating bath stirred. The thickness was 0.1  $\mu\text{m}$ . The test pieces of the coaxial connector 1 were thus completed.

[Table 1]

(Table 1)

Test piece No.	1	2	3	4	5	6
Co content by weight in first metal layer	0	5	10	15	20	25

Each resulting coaxial connector shown in Table 1 was put on a wiring board with a solder having a composition of Sn-3.0Ag-0.5Cu, and was passed through a reflow furnace having a peak temperature of 250°C five times for surface mounting. The rise of the solder after the third passing and the fifth passing through the reflow furnace was observed through a magnifying glass. Also, the shearing strength was measured by applying a pressure to the first principal surface 11 of the test piece after mounting in the

direction parallel to the surface of the wiring board 31 with a push-pull gage. The results are shown in Table 2.

[Table 2]

(Table 2)

Test piece No.	1	2	3	4	5	6
Was there fitting failure by solder rising after 3 cycles of passing through reflow furnace?	Yes	No	No	No	No	No
Was there fitting failure by solder rising after 5 cycles of passing through reflow furnace	Yes	Yes	No	No	No	No
Shearing strength after 5 cycles of passing through reflow furnace	17.9 (1.1)	21.5 (1.6)	19.7 (2.4)	18.7 (1.6)	20.8 (1.2)	-

Each shearing strength is the average derived from 5 test pieces, and the values in the parentheses represent standard deviations  $\sigma_{n-1}$ .

In test piece No. 1 having an x value of less than 5%, which is a comparative example, the solder 32 rose and reached the fitting portion 4 of the coaxial connector 1 in spite of the number of cycles of the passing through the reflow furnace.

In test piece No. 2 having an x value of 5%, which is an example of the present invention, the solder 32 was prevented from rising after three cycles of the passing through the reflow furnace, but the solder 32 rose and reached the fitting portion 4 of the coaxial connector 1 after five cycles of the passing through the reflow furnace.

In test piece Nos. 3, 4, 5, and 6 having x values of

10% to 25%, which are examples of the present invention, the solder 32 was prevented from rising to reach the fitting portion 4 after three cycles and five cycles of the passing through the reflow furnace.

Figs. 3 and 6 are photographs showing the states of the risen solders after five cycles of the passing through the reflow furnace of test piece No. 5 as an example of the present invention and test piece No. 1 as the comparative example, respectively.

The shearing strengths after mounting of test piece Nos. 2 to 6 being the examples of the present invention compared advantageously with the shearing strength of test piece No. 1.

Although the embodiments and the examples illustrate a coaxial connector having a cylindrical fitting portion, the electrical contact component according to the present invention is not limited to this form.

#### Industrial Applicability

As described above, the present invention is useful for surface-mount electrical contact components, such as coaxial connectors, and electrical circuit devices using such electrical contact components. In particular, it is advantageous in preventing solder used for surface mounting from rising to cause fitting failure.